# Dependence of residual voltage ratio behavior of SnO<sub>2</sub>-based varistors on Nb<sub>2</sub>O<sub>5</sub> addition

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 $SnO_2$ -based varistor samples doped with  $Co_2O_3$ ,  $Nb_2O_5$  and  $Cr_2O_3$  were prepared by ball-mixed oxide method. The microstructure, nonlinear *I-V* characteristic and surge current performances of these samples were investigated. This paper mainly focused on the dependence of the residual voltage ratio behavior of  $SnO_2$ -based varistors on  $Nb_2O_5$  addition, different factors influencing the residual voltage ratio in different concentration of  $Nb_2O_5$  were analyzed. The  $Nb_2O_5$  addition influences its residual voltage ratio by changing the grain size, forming defects (especially the free electrons) and cumulative effect. The measured results indicated that the optimally obtained sample with 0.07mol%  $Nb_2O_5$  possesses the lowest residual voltage ratio of 1.86, the corresponding nonlinear coefficient and the threshold electric field are 42.6 and 364.6 V/mm, respectively.

SnO<sub>2</sub>-based varistor, Nb<sub>2</sub>O<sub>5</sub>, residual voltage ratio

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## 1 Introduction

With the unique nonlinear characteristics and high energy handling capabilities, varistors are widely used in electric and electronic systems to suppress the transient overvoltage and absorb surge energy to protect various devices and circuits. Presently, ZnO-based varistor is the prime choice due to its favorable non-ohmic behavior and high energy handling capability. However, as the large doping, ZnO-based varistors contain multiphase which also deteriorate their temperature stability and aging reaction [1–4].

Presently, new varistor materials still have been being explored. In 1995 [5], Pianaro firstly found that  $SnO_2$  ceramics with small amount of doped additives had high density and nonlinear properties. Since then, much attention has been paid to this new material system. In most literatures on SnO<sub>2</sub>-based varistors, the nonlinear coefficient  $\alpha$  is in the range from 8 to 50 [6-10]. Bueno et al. reported that the nonlinear coefficient  $\alpha$  of the varistors composed of 98.95 mol% SnO<sub>2</sub>+1.0 mol% Co<sub>2</sub>O<sub>3</sub>+0.035 mol% Nb<sub>2</sub>O<sub>5</sub>+0.25 mol% Cr<sub>2</sub>O<sub>3</sub>+0.25 mol% La<sub>2</sub>O<sub>3</sub> reached 142 [11]. Same to ZnO,  $SnO_2$  is a kind of n-type semiconductor with rutile structure. But different from the multi-phase structure of the ZnO-based varistors, the SnO<sub>2</sub>-based varistors have simple microstructures. The single-phase structure of this material gives rise to a high stability. Bueno et al. reported that the thermal conductivity of the SnO<sub>2</sub>-based varistor system was two times higher than that of the ZnO-based varistor [12]. It is inferred that, when surge energy was injected into the tested specimens, higher thermal conductivity could improve the temperature uniformity of the ceramic materials and reduce the probability of the thermal-mechanical failure [13], this will also improve their impulse energy absorption capability. In addition, several advantages have been reported for the SnO<sub>2</sub>-based varistors over the ZnO-based

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varistors [14], such as lower additive contents, higher threshold electric field, higher refractivity and better mechanical properties.

However, it is of great challenge for the SnO<sub>2</sub>-based varistors to be utilized in lightning protection systems, concerning with their relatively high residual voltage ratio. Residual voltage ratio is a crucial parameter for a surge protective device that can intuitively reflect varistor overvoltage limiting ability and the nonlinear properties at high current region. It is defined as:  $K_{\rm R} = V_{\rm R}/V_{\rm N}$ , i.e., under 8/20 µs wave, the ratio between the residual voltage under the impulse current of m-kA (normally, m is 5 for 110-kV sure arrester and 10 for 500-kV one) and the voltage under the current DC of 1 mA. Normally the value is smaller than 3 and lower residual voltage ratio will lead to better overvoltage suppressing performance. For this reason, it is expected that a good varistor device should have lower residual voltage ratio. Generally, the residual voltage ratio of commercial ZnO-based varistors is about 1.7, while the value of most SnO<sub>2</sub>-based varistors is more than 2 [13]. If the residual voltage ratio can be lowered further by composition optimizing or new manufacture process, the withstanding capability of the SnO<sub>2</sub>-based varistors to surge current will increase correspondingly.

Despite of its nonlinear coefficient and threshold electric field properties equivalent to the ZnO-based varistors, there is no report in literature with respect to the residual voltage ratio of the SnO<sub>2</sub>-based varistors. Therefore, we drive a study of residual voltage ratio in the SnO<sub>2</sub>-based varistors using 8/20 µs pulse current generator. In this paper we worked on the dependence of the residual voltage ratio behavior of the SnO<sub>2</sub>-based varistors on Nb<sub>2</sub>O<sub>5</sub> addition, the mechanism, and the method reducing the residual voltage ratio ensuring the nonlinear electric properties of the varistors. The Nb<sub>2</sub>O<sub>5</sub> addition influences its residual voltage ratio by changing the grain size, forming defects (especially the free electrons) and cumulative effect. In this paper, we report for the first time the observation of excellent lower residual voltage ratio properties for the SnO<sub>2</sub>-based varistors.

## 2 Experimental procedure

All the oxides used were analytical grade: SnO<sub>2</sub> (99.5%),

 $Co_2O_3$  (99.0%), Nb<sub>2</sub>O<sub>5</sub> (99.99%), Cr<sub>2</sub>O<sub>3</sub> (99.5%). The studied systems correspond to the SnO<sub>2</sub>-based system varistors of composition (99.46-*x*) mol% SnO<sub>2</sub>+0.50 mol% Co<sub>2</sub>O<sub>3</sub>+ 0.04 mol% Cr<sub>2</sub>O<sub>3</sub>+*x* mol% Nb<sub>2</sub>O<sub>5</sub> (*x*=0.05, 0.06, 0.07, 0.08). Samples were prepared by conventional ceramic fabricating processes. SnO<sub>2</sub> powder was blended with additives and ball milled with ethanol. The resulting mixture was cold pressed into round compacts under a pressure of 160 MPa and subsequently sintered at 1300°C for 1 h in air. Ceramic discs with a diameter of about 10 mm and a thickness of about 1.0 mm were obtained. Uniform coating of silver paint was pasted on both sides of the discs as electrodes and was cured at 500°C.

The current-voltage measurements were carried out using HVB4000 (Concept 80 Broadband Dielectric Spectrometer, Novocontrol Technologies GmbH & Co. KG., Germany). The nonlinear coefficient  $\alpha$  was obtained by the equation  $\alpha = \log(I_2/I_1)/\log(V_2/V_1)$  ( $I_1=0.1$  mA,  $I_2=1$  mA were used in this paper). The threshold electric field ( $E_b$ ) was obtained at a current density of 1 mA/cm<sup>2</sup>. The crystalline phase and microstructural graphs were measured by X-ray (D/max-2500) diffraction pattern and scanning electron microscope (JSM-6460LV), respectively. The Nyquist diagram was obtained by using HVB4000, too.

#### **3** Results and discussion

Figure 1 shows the SEM micrographs of different SnO<sub>2</sub>based varistor samples studied here. It was confirmed that we obtained uniform and dense microstructures. Table 1 presents the nonlinear coefficient  $\alpha$ , the threshold electric field  $E_b$ , the leakage current, the residual voltage ratio, the mean grain size, and the relative density. As can be seen, all the systems possess high densities (the relative densities are all above 97%) and present excellent nonlinear I-V characteristics, while the residual voltage ratios are much different. The effects of Nb<sub>2</sub>O<sub>5</sub> concentration on the residual voltage ratio of the SnO<sub>2</sub>-based varistors can be clearly seen from Figure 2. The lowest residual voltage ratio of 1.86 can be obtained when the Nb<sub>2</sub>O<sub>5</sub> concentration is 0.07mol%, which is comparable with that of the ZnO-based varistors. Figure 3 is the Nyquist diagram obtained at 300°C for samples from which the diameters of each semicircle can reflect the resistances of grain boundaries.

Nb <sub>2</sub> O <sub>5</sub> concentration (mol%)	Nonlinear coefficient	$E_b$ (V/mm)	Leakage current (µA)	Residual voltage ratio	Mean grain size (µm)	Relative density (%)
0.05	29.4	415.4	17.6	2.29	3.04	97.5
0.06	29.5	491.2	8.5	2.71	3.11	98.6
0.07	42.6	364.6	1.85	1.86	3.00	98.2
0.08	40.0	198.1	0.19	2.22	2.90	97.0

 Table 1
 Relative density, mean grain size and electrical performance of samples



Figure 1 SEM fractographs of the sintered samples with different concentration ( $x \mod 0$ ) of Nb<sub>2</sub>O<sub>5</sub>. (a) x=0.05; (b) x=0.06; (c) x=0.07; (d) x=0.08.



Figure 2 Relationship between the  $Nb_2O_5$  concentration and the residual voltage ratio of samples.



**Figure 3** Nyquist diagram obtained at  $300^{\circ}$ C for samples with different Nb<sub>2</sub>O<sub>5</sub> concentration *x* mol% (*x*=0.05, 0.06, 0.07, 0.08).

Ions are distributed in different locations for their difference of the ion radius. As  $Co^{2+}$  ions (0.074 nm) are larger than  $Sn^{4+}$  ions (0.071 nm), the substitution of  $Sn^{4+}$  ions by  $Co^{2+}$  ions will lead to significant lattice distortion. As a result, most of the  $Co^{2+}$  ions will stay in the grain boundary and only a spot of the  $Co^{2+}$  ions will leak into the shallow  $SnO_2$  lattice, substitute  $Sn^{4+}$  ions around the grain boundary, and form depletion layer with donors.

$$\text{CoO} \rightarrow \text{Co}_{\text{Sn}}'' + \text{V}_{\text{O}}^{\times} + \text{O}_{\text{O}}^{\times} \tag{1}$$

The production of oxygen vacancies would accelerate the diffusion, and thus promote grain growth.

Since the radius of Nb<sup>5+</sup> ions (0.070 nm) is very close to that of  $Sn^{4+}$  ions (0.071 nm), Nb<sup>5+</sup> ions will replace  $Sn^{4+}$  ions sites and enter the location of the inner grains easily.

$$Nb_2O_5 \rightarrow 2Nb_{sn}^{\cdot} + 2e' + 4O_0^{\times} + 1/2O_2$$
 (2)

$$2Nb_2O_5 \rightarrow 4Nb_{sn} + V_{sn}^{\prime\prime\prime} + 5O_2$$
(3)

In order to reduce the residual voltage ratio, we could extend and flatter the nonlinear zone in the *I-V* curve. It means that more electron carriers are required to participate conducting. Doping Nb<sup>5+</sup> produces a large number of free electrons that can greatly enhance the grain conductivity.

The residual voltage ratio is increased by adding Nb<sub>2</sub>O<sub>5</sub> content in the first stage of the curve in Figure 2. This is because the residual voltage ratio is associated not only with the grain resistance, but also with the grain size. The residual voltage ratio is proportional to the grain size. When the Nb<sub>2</sub>O<sub>5</sub> content is low, more Nb<sup>5+</sup> enter the lattice to replace Sn<sup>4+</sup> with increasing Nb<sub>2</sub>O<sub>5</sub> content, damage the SnO<sub>2</sub> lattice and produce more defects. More defects improve the diffusion of ions, promote grain growth, and ulteriorly in-

crease the residual voltage ratio. At the same time, grain growth and reduction of grain boundaries amounts make the grain boundary resistance lower, as shown in Figure 3.

In the second stage of the curve in Figure 2, the effect of grain growth is no longer important, while the production of large number of free electrons in the crystal reduces the grain resistivity and lowers the corresponding residual voltage obviously. Excess of free electrons will make the grain boundary depletion layer to be weakened or disappear, also reduce the grain boundary resistance as shown in Figure 3.

Nevertheless, when the substitution of Sn<sup>4+</sup> by Nb<sup>5+</sup> becomes saturated, the extra Nb<sup>5+</sup> would not enter SnO<sub>2</sub> lattice any more but accumulate at the grain boundary. These Nb<sup>5+</sup> ions in turn hinder the transport of electrons and other defect ions, which increase the residual voltage ratio and the grain boundary resistance.

Besides residual voltage ratio, other parameters of SnO<sub>2</sub> varistor's electrical properties, for instance, the nonlinear coefficient  $\alpha$ , the threshold electric field  $E_b$ , and the leakage current, are also influenced by Nb<sub>2</sub>O<sub>5</sub> content, as shown in Table 1. Nonlinear coefficient  $\alpha$  heightens following the increase of Nb<sub>2</sub>O<sub>5</sub> content. Figure 4 shows the effect of Nb<sub>2</sub>O<sub>5</sub> content on the nonlinear coefficient  $\alpha$ , the nonlinear coefficient is mainly determined by effective barrier number and the barrier height. At the beginning, the effect of Nb<sub>2</sub>O<sub>5</sub> content on grain growth has little impact on  $\alpha$ . With the increase of Nb<sub>2</sub>O<sub>5</sub> content, a large number of free electrons effectively promote the SnO<sub>2</sub> grains to become semiconducting. The increase in Sn vacancies and other defects help to establish the grain boundary barrier and the nonlinear coefficient is improved consequently. When the Nb<sub>2</sub>O<sub>5</sub> content continues to increase, the reason for the decrease of nonlinear coefficient also is that the extra free electrons in turn make the grain boundary depletion layer to be weakened or disappear. The value of  $E_b$  does not change significantly at the beginning. Whereafter more Nb<sub>2</sub>O<sub>5</sub> additions bring more free electrons which depresses the voltage strength of each grain boundary, and results in the depressed threshold electric field  $E_b$ . Defects caused by Nb<sub>2</sub>O<sub>5</sub> addition accelerate diffusion and promote grain growth, thus help getting more complete and compact grain boundary. Therefore, the leakage current is restricted.

### 4 Conclusions

Based on our research, Nb<sub>2</sub>O<sub>5</sub> concentration has a significant effect on the residual voltage ratio and other nonlinear electrical properties of the SnO<sub>2</sub>-based varistors. With the change of the Nb<sub>2</sub>O<sub>5</sub> content from 0.05 mol% to 0.08 mol%, the residual voltage ratio of samples first increases, then decreases, and at last increases again. In this range, the lowest residual voltage ratio of 1.86 is obtained when the Nb<sub>2</sub>O<sub>5</sub> concentration is 0.07mol%, which is comparable with that of the ZnO-based varistors. It indicates that the



**Figure 4** The nonlinear coefficient  $\alpha$  of SnO<sub>2</sub> variators doped with different Nb<sub>2</sub>O<sub>5</sub> concentration.

 $SnO_2$ -based varistors' residual voltage ratio can be lowered further by optimizing the concentration of  $Nb_2O_5$  and the  $SnO_2$ -based varistors are a kind of promising varistor materials as a potential candidate to compete with the traditional multicomponent ZnO-based varistors.

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- He J L, Hu J, Meng B W, et al. Requirement of ultra-high voltage GIS arrester to voltage gradient of metal-oxide varistor. Sci China Ser E-Tech Sci, 2009, 52(2): 450–455
- 2 Chen Q H, He J L, Tan K X, et al. Influence of grain size on distribution of temperature and thermal stress in ZnO varistor ceramics. Sci China Ser E-Tech Sci, 2002, 45(4): 337–347
- 3 Liu J, Hu J, He J L, et al. Microstructures and characteristics of deep trap levels in ZnO varistors doped with Y<sub>2</sub>O<sub>3</sub>. Sci China Ser E-Tech Sci, 2009 52(12): 3668–3673
- 4 He J L, Hu J, Lin Y H. ZnO varistors with high voltage gradient and low leakage current by doping rare-earth oxide. Sci China Ser E-Tech Sci, 2008, 51(6): 693–701
- 5 Pianaro S A, Bueno P R, Longo E, et al. A new SnO<sub>2</sub>-based varistor system. J Mater Sci Lett, 1995, 14(10): 692–694
- 6 Gupta T K. Application of zin oxide varistors. J Am Ceram Soc, 1990, 73(7): 1817–1840
- 7 Elfwing M, Olsson E. Electron holography study of active interface in zinc oxide varistor materials. J Appl Phys, 2002, 92(9): 5272–5280
- Clarke D R. Varistor ceramics. J Am Ceram Soc, 1999, 82(3): 485–502
   Santhosh P N, Date S K. A new composition of ceramic varistor:
- SnO<sub>2</sub> doped with (Co, Nb, Al). Bull Mater Sci, 1996, 19(4): 713–715 Peiteado M, De la Rubia M A, Velasco M J, et al. Bi<sub>2</sub>O<sub>3</sub> vaporization
- from ZnO-based varistors. J Eut Ceram Soc, 2005, 25(9): 1675–1678 11 Bueno P R, Olivera M M, Bacelar W K, et al. Analysis of the admit-
- tance-frequency and capacitance-voltage of dense SnO<sub>2</sub>-CoO-based varistor ceramics. J Appl Phys, 2002, 91(9): 6007–6014
  Bueno P R, Varela J A, Barrado C M, et al. A comparative study of
- 12 Bueno P R, Varela J A, Barrado C M, et al. A comparative study of thermal conductivity in ZnO- and SnO<sub>2</sub>-based varistor systems. J Am Ceram Soc, 2005, 88(9): 2629–2631
- 13 Lu Z Y, Chen Z W, Wu J Q. SnO<sub>2</sub>-based varistor capable of withstanding surge current. J Ceram Soc Jpn, 2009, 117(7): 851–855
- 14 Ramirez M A, Bassi W, Parra R, et al. Comparative electrical behavior at low and high current of SnO<sub>2</sub>- and ZnO-based varistors. J Am Ceram Soc, 2008, 91(7): 2402–2404